

# Mathematical Modeling

## CSTR Example

# Develop a Dynamic Model

- Draw a schematic diagram, labeling process variables
- List all assumptions
- Classify Problem
  - Time Dependence Only
    - ODE: Ordinary differential equations
    - DAE: Differential algebraic equations
  - Time and Spatial Dependence
    - PDE: Partial differential equations
    - PDAE: Partial differential algebraic equations
- Write dynamic balances (mass, species, energy)
- Other relations (thermo, reactions, geometry, etc.)
- Degrees of freedom
  - Does # of eqns = # of unknowns?
- Simplify

# Balances

- **Total Mass Balance:**

$$\frac{dm}{dt} = \frac{d(\rho V)}{dt} = \sum_{i=\text{inlet}} \dot{m}_i - \sum_{j=\text{outlet}} \dot{m}_j$$

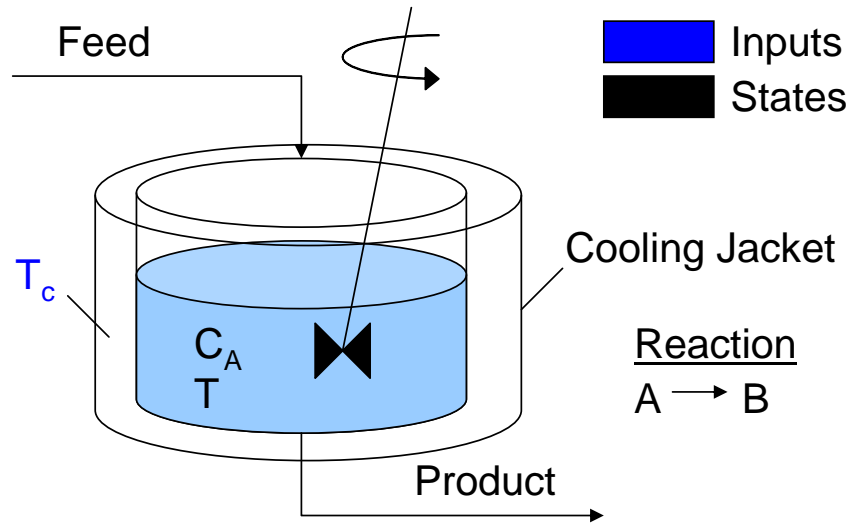
- **Species Mole Balance:**

$$\frac{dn_A}{dt} = \frac{d(c_A V)}{dt} = \sum_{i=\text{inlet}} c_{Ai} q_i - \sum_{j=\text{outlet}} c_{Aj} q_j + r_A V$$

- **Total Energy Balance:**

$$\frac{d[\rho C_p V (T - T_{ref})]}{dt} = \sum_{i:\text{inlet}} \dot{m}_i C_p (T_i - T_{ref}) - \sum_{j:\text{outlet}} \dot{m}_j C_p (T_j - T_{ref}) + Q + W_s$$

# Process Diagram



## Assumptions

1. Liquid-only system
2. Constant volume (tight level control)
3. First Order Reaction
4. No Jacket Temperature Dynamics
5. Negligible Heat Input from Stirring
6. Constant Density

# Process Information

<b>Manipulated Variables</b>	
$T_c = 270$	Temperature of cooling jacket (K)
<b>Disturbances</b>	
$q = 100$	Volumetric Flowrate ( $\text{m}^3/\text{sec}$ )
$V = 100$	Volume of CSTR ( $\text{m}^3$ )
$\rho = 1000$	Density of A-B Mixture ( $\text{kg}/\text{m}^3$ )
$C_p = .239$	Heat capacity of A-B Mixture ( $\text{J}/\text{kg}\cdot\text{K}$ )
$m\Delta H = 5e4$	Heat of reaction for A $\rightarrow$ B ( $\text{J}/\text{mol}$ )
$E_{\text{overR}} = 8750$	$E_{\text{overR}} = E/R =$ Activation energy ( $\text{J}/\text{mol}$ ) / Universal Gas Constant ( $8.31451 \text{ J}/\text{mol}\cdot\text{K}$ )
$k_0 = 7.2e10$	Pre-exponential factor ( $1/\text{min}$ )
$UA = 5e4$	$UA = U * A =$ Overall Heat Transfer ( $\text{W}/\text{m}^2\cdot\text{K}$ ) / Area ( $\text{m}^2$ )
$C_{af} = 1$	Feed Concentration ( $\text{mol}/\text{m}^3$ )
$T_f = 350$	Feed Temperature (K)
<b>Differential States</b>	
$C_a = 0.9$	Concentration of A in CSTR ( $\text{mol}/\text{m}^3$ )
$T = 305$	Temperature in CSTR (K)

# Model Equations

## Species Mole Balance for Component A

$$\frac{dn_A}{dt} = \frac{d(c_A V)}{dt} = \sum_{i=\text{inlet}} c_{Ai} q_i - \sum_{j=\text{outlet}} c_{Aj} q_j + r_A V$$

$$V \frac{dc_A}{dt} = c_{A.in} q - c_A q + r_A V$$

## Energy Balance

$$\frac{d[\rho C_p V (T - T_{ref})]}{dt} = \sum_{i:\text{inlet}} \dot{m}_i C_p (T_i - T_{ref}) - \sum_{j:\text{outlet}} \dot{m}_j C_p (T_j - T_{ref}) + Q + W_s$$

$$\rho C_p V \frac{dT}{dt} = \rho C_p q (T_{in} - T) + r_A \Delta H_r - UA(T - T_C)$$

## Other Equation(s): Reaction Rate

$$r_A = k_0 c_A \exp\left(-\frac{E}{RT}\right)$$

# Degrees of Freedom

## Number of Variables

$$c_A \quad T \quad r_A$$

## Number of Equations

$$V \frac{dc_A}{dt} = c_{A.in} q - c_A q + r_A V$$

$$\rho C_p V \frac{dT}{dt} = \rho C_p q (T_{in} - T) + r_A \Delta H_r - UA(T - T_C)$$

$$r_A = k_0 c_A \exp\left(-\frac{E}{RT}\right)$$

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$$N_{DOF} = N_{Variables} - N_{Equations}$$

# Simplify

## Variables

$c_A$   $T$   ~~$r_A$~~

Substitute

$$r_A = k_0 c_A \exp\left(-\frac{E}{RT}\right)$$

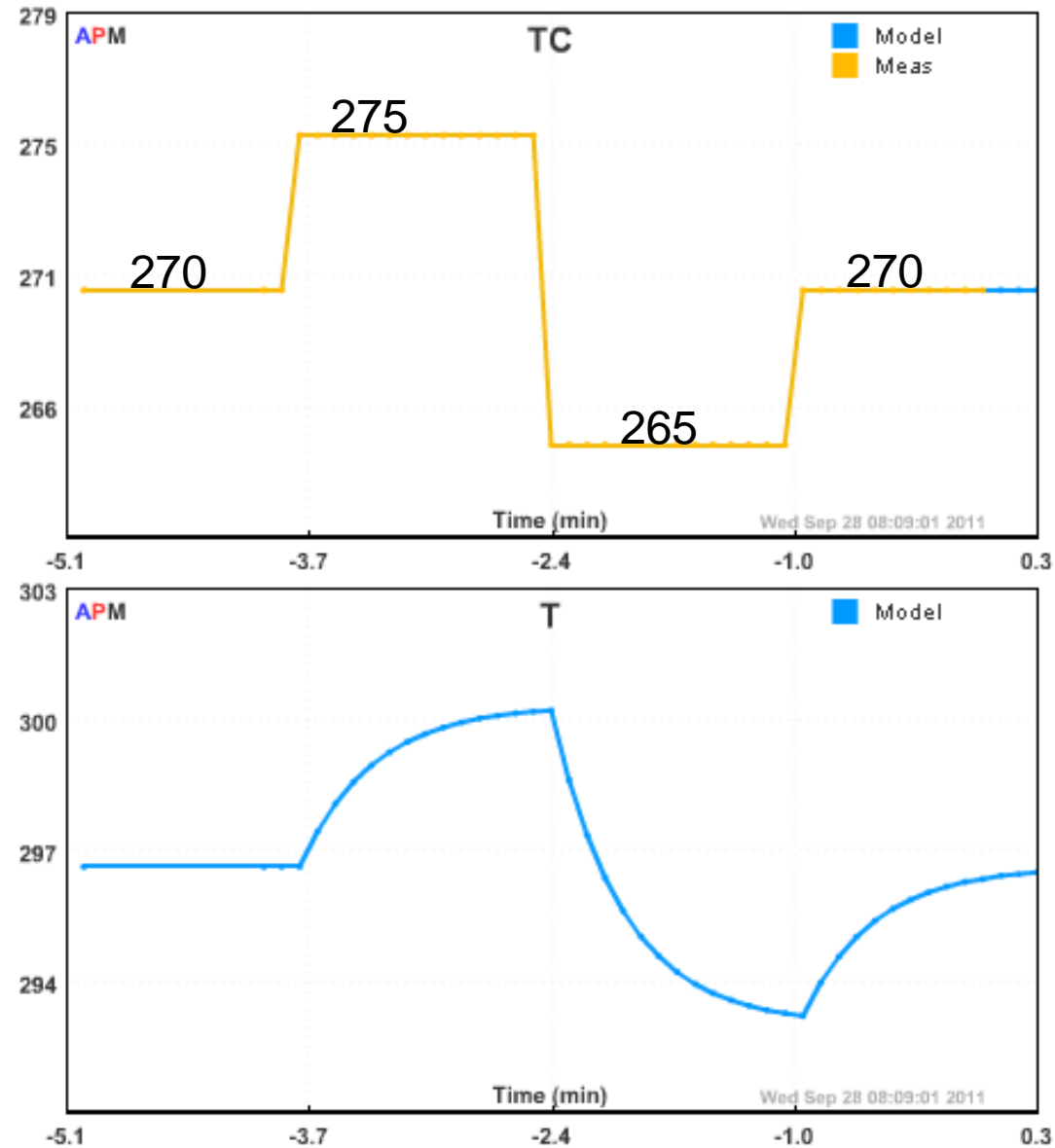
## Equations

$$V \frac{dc_A}{dt} = c_{A.in} q - c_A q + r_A V$$

$$\rho C_p V \frac{dT}{dt} = \rho C_p q (T_{in} - T) + r_A \Delta H_r - UA(T - T_C)$$

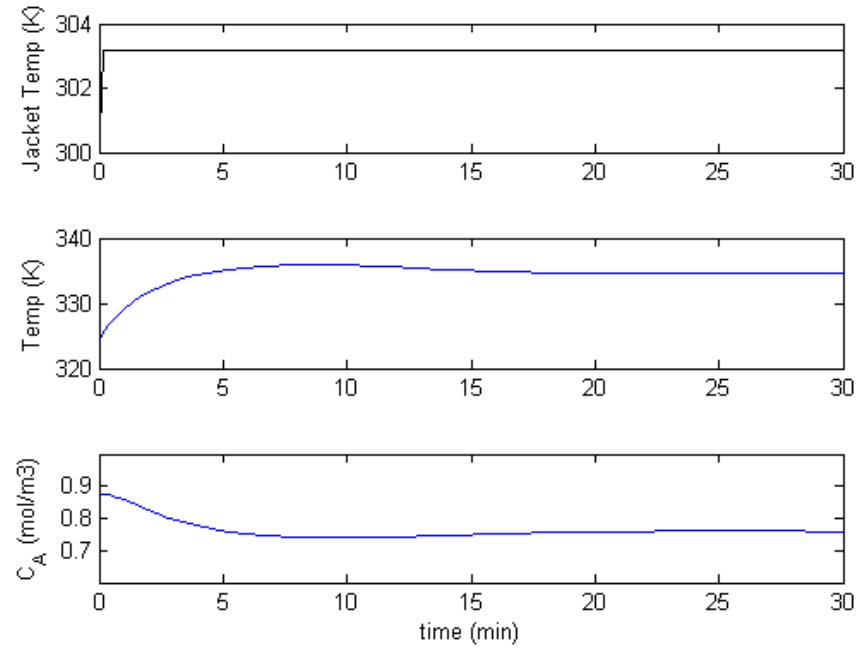


# Simulate: Doublet Test

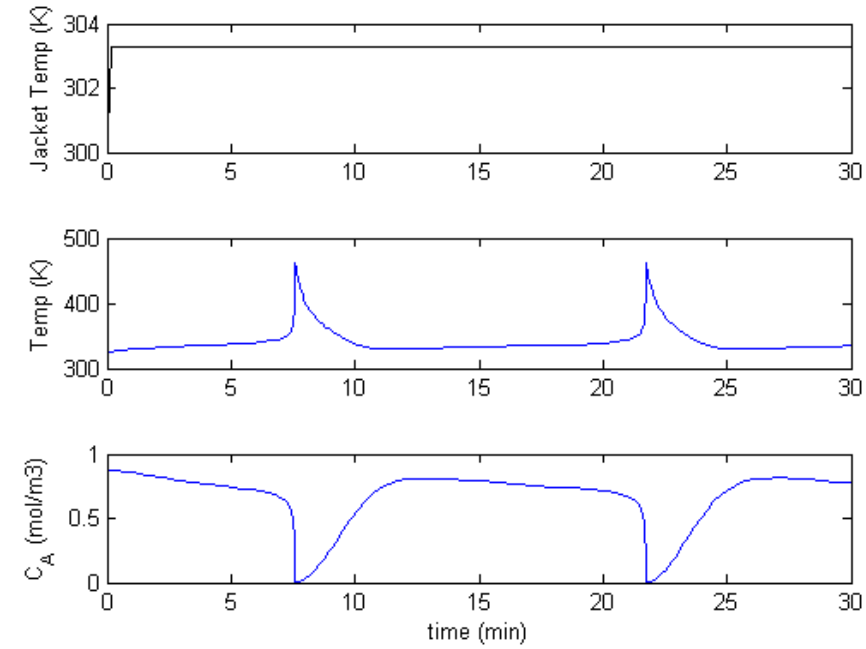


# Stability Analysis

$T_c = 303.2 \text{ K}$



$T_c = 303.3 \text{ K}$



# Model-Based Control

How does the controller achieve 380 K when manual control to 335 K appeared to cause run-away reaction?

